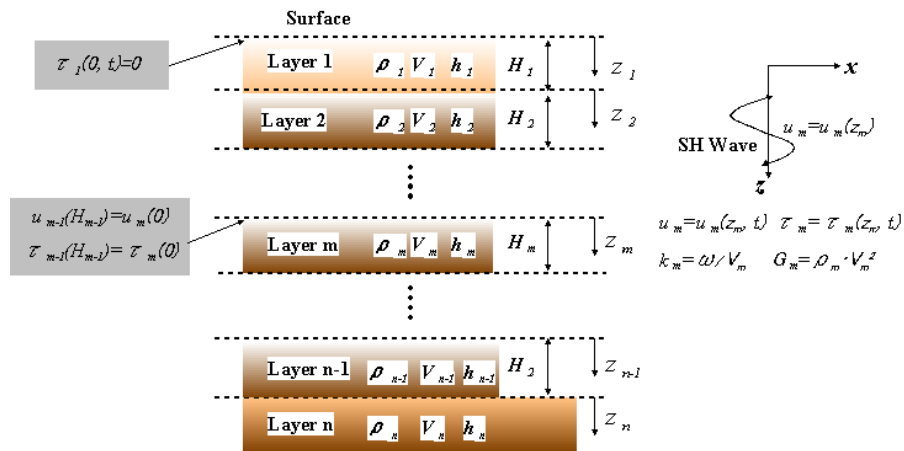
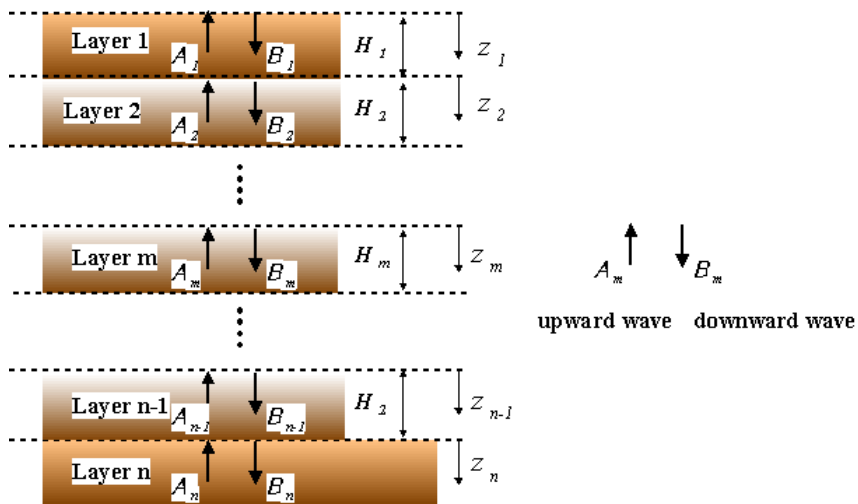


Multi-reflection theory for one-dimensional wave in multi-layers system



Multi-Layer System and Coordinate System



Reflection and Refraction

$$\rho \frac{\partial^2 u}{\partial t^2} = G \frac{\partial}{\partial z} (\gamma) + c \frac{\partial}{\partial z} \left( \frac{\partial \gamma}{\partial t} \right) = G \frac{\partial^2 u}{\partial z^2} + \eta \frac{\partial^3 u}{\partial z^2 \partial t} \quad : \text{ refer to Navier-Stokes Equation for viscous fluid} \quad (A)$$

$$\eta = \frac{G}{\omega} 2h \quad : h \text{ is damping factor.} \quad (B)$$

$$u(z, t) = \exp \left[ i\omega \left( t - \frac{z}{V_s^*} \right) \right], \text{ here, } V_s^* \text{ indicates shear velocity with account for viscosity} \quad (C)$$

Substituting (C) into (A), we can obtain,

$$\rho (V_s^*)^2 = G + i\eta\omega \quad (D)$$

$$V_s^* = \sqrt{G + i\eta\omega} = V_s \sqrt{G + i\eta\omega/G} \quad : \text{ complex shear velocity} \quad (E)$$

where,  $\eta\omega/G$  is usually small so that it could be negligible, so we apply Taylor's expansion to (E) and then (E) reduce to

$$\frac{1}{V_s^*} \approx \frac{1}{V_s} \left( 1 - \frac{1}{2} i \frac{\omega\eta}{G} \right) \quad (F)$$

Substituting (F) into (C), we can obtain,

$$u(z, t) = \exp \left[ i\omega \left( t - \frac{z}{V_s} \right) \right] \exp \left[ -\frac{\eta\omega^2 z}{2V_s G} \right] \quad (G)$$

This solution means that wave is attenuated while propagating with velocity of  $V_s$  and the damping is exponential term which is proportional to  $\eta$ .

$$\text{Otherwise, logarithm damping ratio } \delta = \ln \left( \frac{a_1}{a_2} \right) = \ln \left( \frac{a_2}{a_3} \right) = \dots = 2\pi h. \quad \Rightarrow \text{ eq.(B)}$$

Therefore, displacement can be described as

$$u(z, t) = \exp \left[ i\omega \left( t - \frac{z}{V_s} \right) \right] \exp \left[ -\frac{2\pi h \cdot z}{\lambda G} \right] \quad \left( \lambda = \frac{2\pi V_s}{\omega} : \text{ wave length} \right) \quad (H)$$

When we use  $G^*$ , (A) can be rewritten by the following equation.

$$\rho \frac{\partial^2 u}{\partial t^2} = G^* \frac{\partial^2 u}{\partial z^2} \quad (I)$$

$$G^* = G(1 + i2h) \quad : \text{ complex shear modulus} \quad (J)$$

( one of empirical relations:  $h \approx 0.017 + 0.0002 V_s$  )

1) Upward wave and Downward wave with only SH component in Horizontal Layers

Displacement function in the  $m$ -th layer

$$u_m(z_m, t) = A_m \exp[i(k_m z_m + \omega t)] + B_m \exp[i(k_m z_m - \omega t)] \quad (4.1)$$

$$k_m = \frac{\omega}{V_m} = \frac{2\pi}{\lambda_m} : \text{wave number } (V_m = f\lambda_m = \frac{\omega}{2\pi} \lambda_m) \quad (4.2)$$

$$V = V^{\text{Re}} \sqrt{1 + ic\omega} : \text{complex velocity} \quad (4.3)$$

$$G \approx G^{\text{Re}}(1 + i2h) : \text{complex shear modulus} \quad (4.4)$$

Shear stress – shear strain described by displacement fields

$$\gamma = \frac{\partial u_m}{\partial z_m} = ik_m [A_m \exp\{i(k_m z_m + \omega t)\} - B_m \exp\{-i(k_m z_m - \omega t)\}] \quad (4.5)$$

$$\tau_m(z_m, t) = iG_m k_m [A_m \exp\{i(k_m z_m + \omega t)\} - B_m \exp\{-i(k_m z_m - \omega t)\}] \quad (4.6)$$

Matrix description in  $m$ -th layer for amplitude

$$\begin{Bmatrix} u_m(z_m) \\ \tau_m(z_m) \end{Bmatrix} = \begin{bmatrix} \exp(ik_m z_m) & \exp(-ik_m z_m) \\ iG_m k_m \exp(ik_m z_m) & -iG_m k_m \exp(-ik_m z_m) \end{bmatrix} \begin{Bmatrix} A_m \\ B_m \end{Bmatrix} \quad (4.7)$$

at  $z_m = 0$

$$\begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} = \begin{bmatrix} 1 & 1 \\ iG_m k_m & -iG_m k_m \end{bmatrix} \begin{Bmatrix} A_m \\ B_m \end{Bmatrix} \quad (4.8)$$

at  $z_m = z_m$

$$\therefore \begin{Bmatrix} u_m(z_m) \\ \tau_m(z_m) \end{Bmatrix} = \begin{bmatrix} \cos k_m z_m & \frac{\sin k_m z_m}{G_m k_m} \\ -G_m k_m \sin k_m z_m & \cos k_m z_m \end{bmatrix} \begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} \quad (4.9)$$

at  $z_m = H_m$

$$\therefore \begin{Bmatrix} u_m(H_m) \\ \tau_m(H_m) \end{Bmatrix} = [S_m] \begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} \quad (4.10)$$

$$[S_m] = \begin{bmatrix} \cos k_m H_m & \frac{\sin k_m H_m}{G_m k_m} \\ -G_m k_m \sin k_m H_m & \cos k_m H_m \end{bmatrix} \begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} \quad (4.11)$$

Boundary condition at the interface between  $(m-1)$ th and  $m$ -th layers

$$\text{at } z_{m-1} = H_{m-1} \text{ and } z_m = 0 \begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} = \begin{Bmatrix} u_{m-1}(H_{m-1}) \\ \tau_{-1}(H_{m-1}) \end{Bmatrix} \quad (4.12)$$

$$\begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} = [S_{m-1}] \begin{Bmatrix} u_{m-1}(0) \\ \tau_{m-1}(0) \end{Bmatrix} \quad (4.13)$$

*Recurrence formulation for amplitude in m-th layer assessed by that of 1st layer*

$$\begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} = [R_{m-1}] \begin{Bmatrix} u_1(0) \\ \tau_1(0) \end{Bmatrix} \quad (4.14)$$

$$\left( \begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} = [S_{m-1}] \begin{Bmatrix} u_{m-1}(0) \\ \tau_{m-1}(0) \end{Bmatrix} = [S_{m-1}] [S_{m-2}] \begin{Bmatrix} u_{m-2}(0) \\ \tau_{m-2}(0) \end{Bmatrix} = \dots \right)$$

where,

$$[R_{m-1}] = [S_{m-1}] [S_{m-2}] \dots [S_1] \quad (4.15)$$

at the ground surface:  $z_1 = 0$

$$\tau_1(0) = 0 \quad (4.16)$$

Therefore,

$$\therefore \begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} = [R_{m-1}] \begin{Bmatrix} u_1(0) \\ 0 \end{Bmatrix} \quad (4.17)$$

The above results are summarized as follows:

$$\left. \begin{aligned} \begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} &= [R_{m-1}] \begin{Bmatrix} u_1(0) \\ 0 \end{Bmatrix} \\ \begin{Bmatrix} u_m(z_m) \\ \tau_m(z_m) \end{Bmatrix} &= \begin{bmatrix} \cos k_m z_m & \frac{\sin k_m z_m}{G_m k_m} \\ -G_m k_m \sin k_m z_m & \cos k_m z_m \end{bmatrix} \begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} \end{aligned} \right\} \quad (4.18)$$

**2) Frequency Response Function (周波数応答関数)**

From Eq.(4.1),

$$\begin{Bmatrix} A_n \\ B_n \end{Bmatrix} = \frac{1}{2} \begin{bmatrix} 1 & -\frac{i}{G_n k_n} \\ 1 & \frac{1}{G_n k_n} \end{bmatrix} \begin{Bmatrix} u_n(0) \\ \tau_n(0) \end{Bmatrix} \quad (4.19)$$

$$\begin{cases} u_n(0) = \mathbf{R}_{n-1}(1, 1)u_1(0) \\ \tau_n(0) = \mathbf{R}_{n-1}(2, 1)u_1(0) \end{cases} \quad (4.20)$$

$$A_n = \frac{u_1(0)}{2} \left[ \mathbf{R}_{n-1}(1, 1) - i \frac{\mathbf{R}_{n-1}(2, 1)}{G_n k_n} \right] \quad (4.21)$$

$$U_1(\omega) = \frac{2}{\sqrt{[\mathbf{R}_{n-1}(1, 1)]^2 + [\mathbf{R}_{n-1}(2, 1)/G_n k_n]^2}} \quad (4.22)$$

3) Amplification Factor (増幅率)

From Eq.(4.13) and Eq.(4.14)

$$\begin{Bmatrix} A_m \\ B_m \end{Bmatrix} = [T_{m-1}] \begin{Bmatrix} A_{m-1} \\ B_{m-1} \end{Bmatrix} \quad (4.23)$$

$$[T_{m-1}] = \begin{bmatrix} \frac{1}{2}(1 + \alpha_{m-1})\exp(ik_{m-1}H_{m-1}) & \frac{1}{2}(1 - \alpha_{m-1})\exp(-ik_{m-1}H_{m-1}) \\ \frac{1}{2}(1 - \alpha_{m-1})\exp(ik_{m-1}H_{m-1}) & \frac{1}{2}(1 + \alpha_{m-1})\exp(-ik_{m-1}H_{m-1}) \end{bmatrix} \quad (4.24)$$

where

$$\alpha_{m-1} = \frac{G_{m-1}k_{m-1}}{G_m k_m} = \frac{\rho_{m-1}V_{m-1}}{\rho_m V_m} \quad (4.25)$$

$\rho_m V_m$  is wave impedance(波動インピーダンス)

$\alpha$  is impedance ratio

From Eq.(4.8) and Eq.(4.17), we can obtain the following relation,

$$\begin{Bmatrix} u_m(0) \\ \tau_m(0) \end{Bmatrix} = \begin{bmatrix} 1 & 1 \\ iG_m k_m & -iG_m k_m \end{bmatrix} \begin{Bmatrix} A_m \\ B_m \end{Bmatrix} \quad (4.7)'$$

$$\tau_1(0) = 0 \quad (4.16)$$

the following relation is obtained

$$A_1 = B_1 \quad (\text{from Eq.(4.7)' and Eq.(4.16)}) \quad (4.26)$$

$$u_1(0) = 2A_1 \quad (\text{from Eq.(4.7)' and Eq.(4.26)}) \quad (4.27)$$

Amplitude in  $m$ -th layer assessed by that of 1st layer

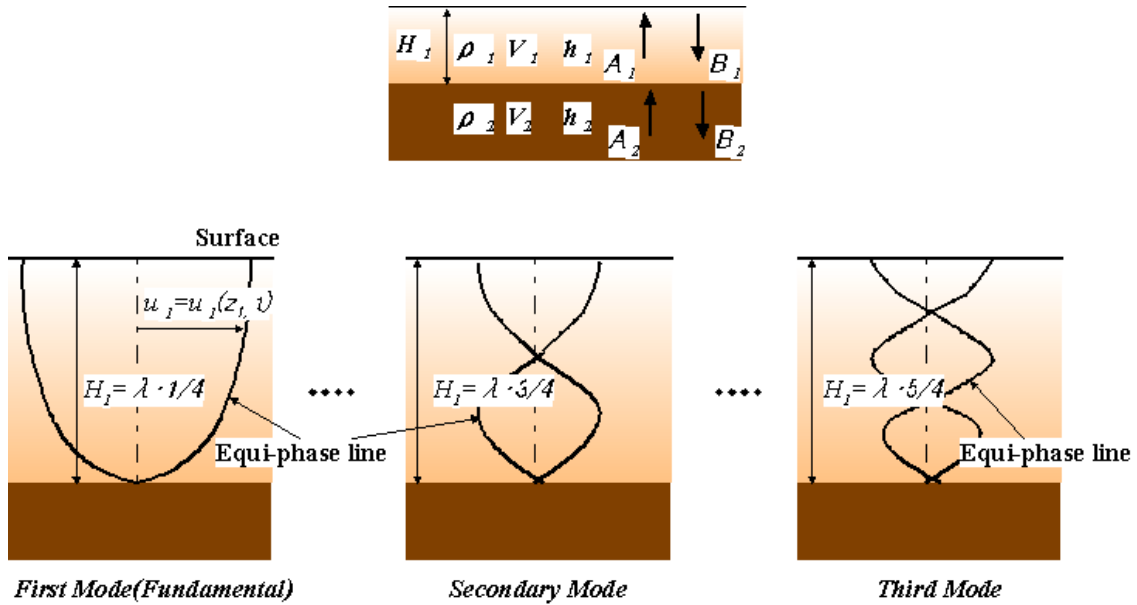
$$\begin{Bmatrix} A_m \\ B_m \end{Bmatrix} = [Q_{m-1}] \begin{Bmatrix} A_1 \\ A_1 \end{Bmatrix} \quad (4.28)$$

where,

$$[Q_{m-1}] = [T_{m-1}][T_{m-2}] \cdots [T_1] \quad (4.29)$$

4) Fundamental consideration in two-layer system

Resonance and sympathetic vibration in tow-layer system



Geometries in resonance of two layer system

For two layers,

[ Amplification ]

$$A_1 = B_1 = \frac{1}{\cos(k_1 H_1) + i \alpha_1 \sin(k_1 H_1)} A_2 \quad (a)$$

$$B_2 = \frac{\cos(k_1 H_1) - i \alpha_1 \sin(k_1 H_1)}{\cos(k_1 H_1) + i \alpha_1 \sin(k_1 H_1)} A_2 \quad (b)$$

[ Natural Period(Frequency) ]

$$\cos k_1 H_1 = 0$$

$$\omega_n = 2\pi f_n = 2\pi \frac{V_1}{\lambda_n} = 2\pi V_1 \frac{1}{\left( \frac{H_1}{(2l-1)} \right)} = (2l-1) \frac{\pi V_1}{2H_1} \quad (l=1, 2, \dots)$$

$$H_1 = \frac{\lambda_1}{4} (2l-1), \quad V_1 = f \lambda_1 = f \frac{4}{(2l-1)} H_1$$

$$T_n = \frac{2\pi}{\omega_n} = \frac{1}{f} = V_1 \frac{(2l-1)}{4H_1} \quad (c)$$

[ Energy ]

$$E = \frac{1}{2} \rho \cdot V \cdot \omega^2 \cdot |A|^2 \quad (d)$$

Propagation energy per unit time

kinematics

$$(E_K)_{\max} = \left[ \frac{1}{2} m \cdot V^2 \right] = \frac{1}{2} \rho V_s \cdot (V)^2 = \frac{1}{2} \rho V \cdot (\omega |A|)^2$$

potential

$$(E_U)_{\max} = \left( \frac{1}{2} G \cdot \gamma_{\max}^2 \right) \cdot V_s = \left( \frac{1}{2} \rho V_s^2 \cdot (k|A|)^2 \right) \cdot V = \left( \frac{1}{2} \rho V_s^2 \cdot \frac{\omega^2}{V_s^2} |A|^2 \right) \cdot V_s$$

If a wave propagates from hard material to soft material ( $V_s$  decreases), the amplitude increases under constant energy.

$$\frac{E_T}{E_0} = \frac{\alpha_1}{\cos^2(k_1 H_1) + \alpha_1^2 \sin^2(k_1 H_1)} \quad (e)$$

$$\frac{E_T}{E_0} = 1$$

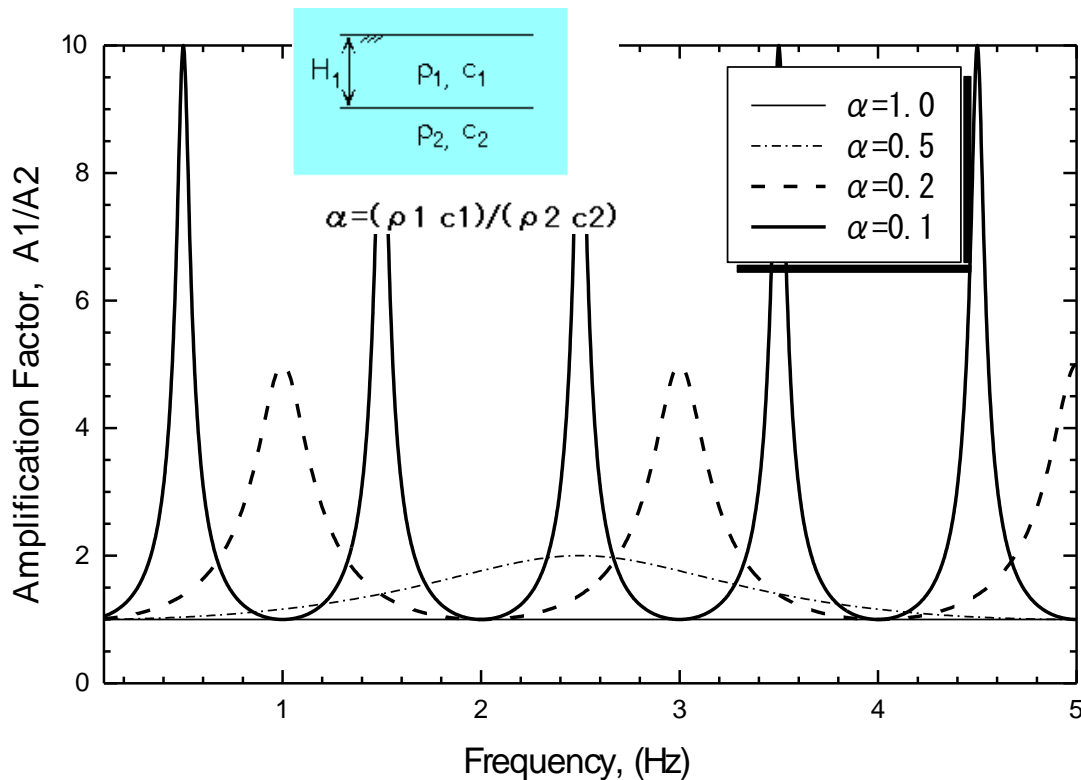
For multi-layers,

[ Natural Period(Frequency) ] Simple approximations

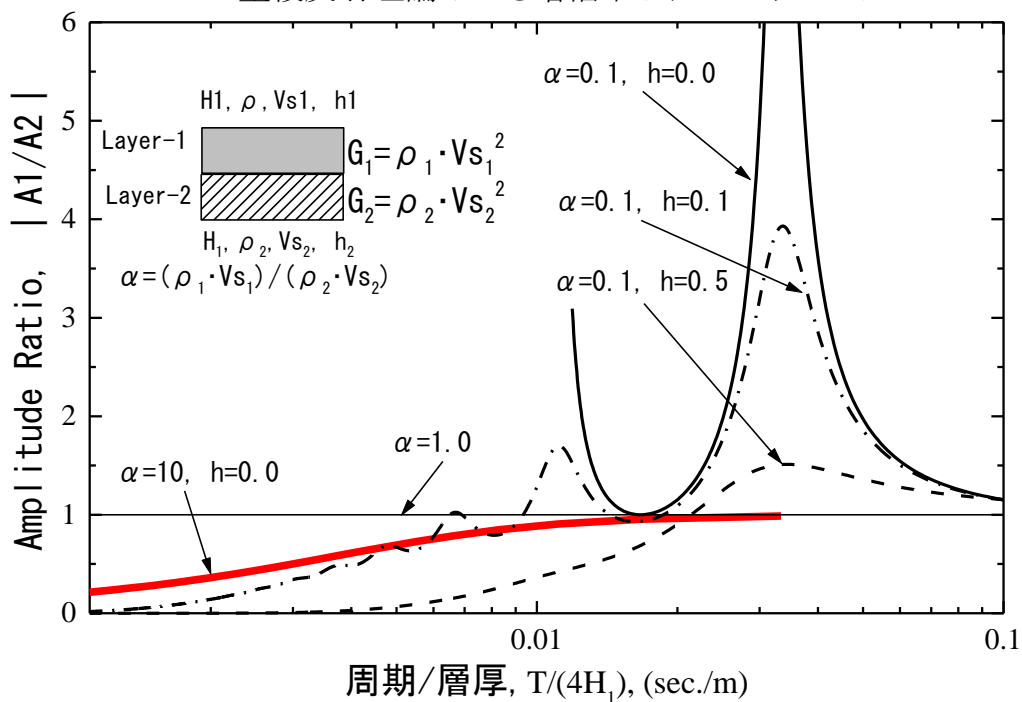
$$(i) \quad T = \frac{\lambda_1}{V_1} + \dots + \frac{\lambda_n}{V_n} = \frac{4H_1}{V_1} + \dots + \frac{4H_n}{V_n} = \sum_{j=1}^n \frac{4H_j}{V_j}$$

$$(ii) \quad T = \frac{4 \sum_{j=1}^n H_j}{V_{ave}}, \quad V_{ave} = \frac{\sum_{j=1}^n V_j H_j}{\sum_{j=1}^n H_j}$$





重複反射理論 による増幅率とインピーダンス比



Examples for seismic isolation effect

